

Fast Aeroelastic Assessment Methods for Industrial Aircraft Design

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iPhD Project

About

- University of Southampton, south coast UK
- Next Generation Computational Modelling (NGCM) iPhD
 - ▶ Taught 1st year, scientific computation methods
 - ▶ 3 years of research
- Funded by Engineering and Physical Sciences Research Council



Outline

1

Overview

- Aims
- Methods

2

Results

- Progress
- Validation/Results

3

Summary

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Summary

Aims

- Collaboration with Airbus UK
- Improved fidelity rapid method for aeroelastic loads assessment
- Bridge gap between CFD and linear methods
- Early in the design process
- Produce results overnight

Motivation

- Aeroelasticity (Gust response, Flutter..) is a threat for flexible aircraft.



NASA Helios Mishap ¹. Left: Pitching oscillations and dihedral angles beyond design limit (aeroelastic response).
Right: Structural disintegration resulting from critical loads

¹ Noll, T. et al, "Investigation of the Helios Prototype Aircraft Mishap: Volume I Mishap Report,"
<http://www.nasa.gov>. Jan 2004

Applications

- Aircraft design, optimisation
- Flow control research
- Study of aeroelastic phenomena
- Agile vehicle research

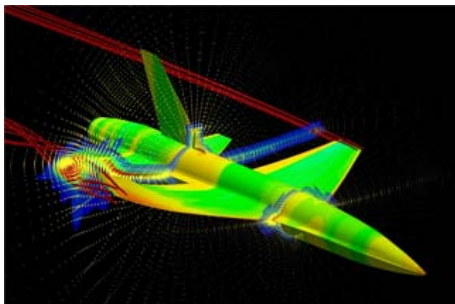


Figure 1: Aeroelastic modelling of a fighter aircraft ²

²Patrick Hu, Source: <http://www.advanceddynamics-usa.com/>

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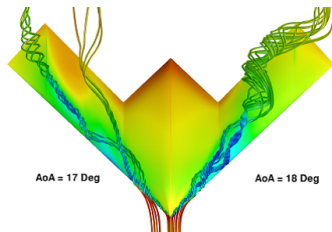
Summary

Aerodynamic Methods

- Unsteady Vortex Lattice Method (UVLM) - 3D inviscid
- Reynolds Averaged Navier Stokes (RANS), Infinite Swept Wing - '2.5D+' viscous
- Iterative ' α correction' method for viscous/inviscid coupling
- Implemented in solver code 'Tau' (C Programming language)

Alternative: Doublet Lattice Method

- Frequency Domain Approach
- Available in most aeroelasticity packages (e.g. NASTRAN)
- Fast **linear** Method
- Insufficient for non-linear flows



Late stages of vortex with breakdown occurring over the top surface of SACCON³

³Vallespin, D., Da Ronch, A., Boelens, O. and Badcock, K. J. (2011) Vortical flow prediction validation for an unmanned combat air vehicle model. Journal of Aircraft, 48, (6), 1948-1959.

UVLM

-
- The diagram illustrates a wing wake model. A wing is shown in a 3D coordinate system with axes x , y , and z . The wing's trailing edge is at the origin 0 . The wing is divided into sections labeled j , $j+1$, and $j+2$ along the y -axis, and i , $i+1$, and $i+2$ along the x -axis. The wing's orientation is defined by angles ψ (yaw) and ϕ (roll). The wing's velocity components are $U(t)$, $V(t)$, and $W(t)$. The wake is represented by a series of rectangular panels (wake panels) extending from the trailing edge. The location of the trailing edge at time $t = t_0$ is indicated. The wake panels are shown at different times: $t_0 - \Delta t$, $t_0 - 2\Delta t$, and $t_0 - 3\Delta t$. The wake panels are labeled j , $j+1$, and $j+2$ along the y -axis, and i , $i+1$, and $i+2$ along the x -axis. The wake panels are shown at different times: $t_0 - \Delta t$, $t_0 - 2\Delta t$, and $t_0 - 3\Delta t$. The wake panels are labeled j , $j+1$, and $j+2$ along the y -axis, and i , $i+1$, and $i+2$ along the x -axis. The wake panels are shown at different times: $t_0 - \Delta t$, $t_0 - 2\Delta t$, and $t_0 - 3\Delta t$. The wake panels are labeled j , $j+1$, and $j+2$ along the y -axis, and i , $i+1$, and $i+2$ along the x -axis. The wake panels are shown at different times: $t_0 - \Delta t$, $t_0 - 2\Delta t$, and $t_0 - 3\Delta t$. The wake panels are labeled j , $j+1$, and $j+2$ along the y -axis, and i , $i+1$, and $i+2$ along the x -axis.

Viscous Inviscid Coupling (steady state)

- Infinite Swept Wing⁵:
 - ▶ Spanwise decoupled RANS
 - ▶ Sectional viscous data lookup table C_L vs α
- Coupling: α correction^{6 7}:
 - ▶ VLM \rightarrow inviscid lift coefficient $C_{L_{inv}}$, effective angle of attack α_{eff}
 - ▶ $\alpha_{eff} \rightarrow C_{L_{visc}}$
 - ▶ $\Delta\alpha = (C_{L_{visc}} - C_{L_{inv}}) / C_{L_{\alpha, visc}}$
 - ▶ Correct α_{eff} , iterate to convergence in $|C_{L_{visc}} - C_{L_{inv}}|$

⁵ Ghasemi et al. "A Two-Dimensional Infinite Swept Wing Navier-Stokes Solver," 52nd Aerospace Sciences Meeting, AIAA SciTech, Jan. 2014.

⁶ Van Dam, C. P., "The aerodynamic design of multi-element high-lift systems for transport airplanes" Progress in Aerospace Sciences, Vol. 38, No. 2, 2002, pp. 101-144.

⁷ Galloway, S. et al., "Sweep effects on non-linear Lifting Line Theory near Stall" 52nd Aerospace Sciences Meeting, AIAA SciTech, Jan. 2014.

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Progress

- Steady VLM code implemented in C
- Some code validation
- Version control and testing
- Spanwise decoupled (ISW) RANS algorithm generated in Tau

Code structure

- Lifting surface object orientation, with attributed wake
- Multiple surface 'objects' support
- HDF5 file format read/write
 - ▶ CGNS based on HDF5
 - ▶ Supports large data sets with objects and attributes
 - ▶ File compression
- Fast LAPACK libraries for solving linear systems

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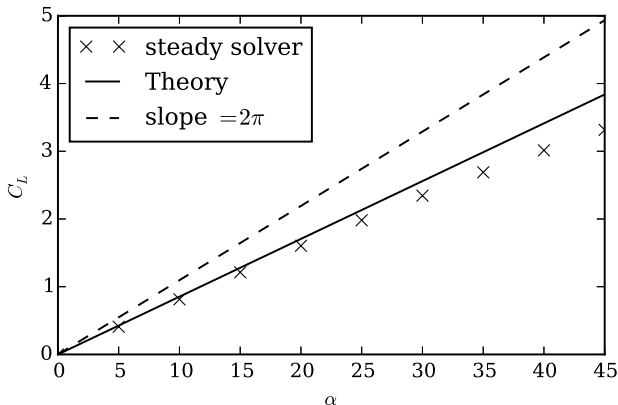
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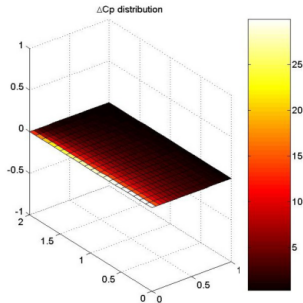
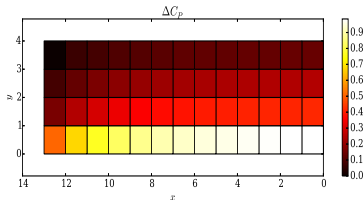
VLM Validation

- Compare with finite wing theory -

$$C_{L_{\alpha_wing}} = \frac{C_{l_{\alpha}}}{1 + \frac{C_{l_{\alpha}}}{\pi e AR}}$$



Results



Pressure distribution

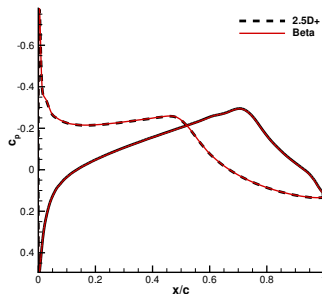
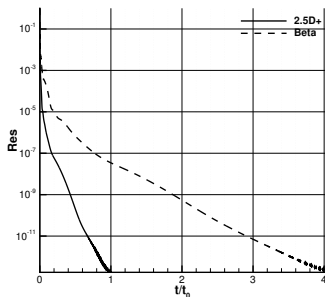
Left: VLM result

Right: DLM result, low reduced frequency ($k = 0.1$)⁸

⁸ Da Ronch A., Cavagna, L. "A Doublet-Lattice Method for Calculating Lift Distributions on Planar and Non-Planar Configurations in Subsonic Flows", May 2007.

Progress

- Speedup factor of around 4 with 2.5D+ method compared with Tau standard method



Left: Convergence history speedup demonstration

Right: Pressure coefficient comparison

To Be Implemented...

- Extension of α correction method and VLM to unsteady flight mechanics
- Fast multipole algorithm (wake)
- Eigenvalue modal decomposition for structural response (NASTRAN)
- Test case using non-confidential data, DLR-F6 wing-body

Summary

- Improved fidelity fast aeroelastic method
- Target vulnerable aircraft early in design
- Aerodynamic model: 3D UVLM coupled with 2D RANS
- Structural model: Modal approach

Thank you.